

# Cryogenic

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### Abstract

Why do we adopt cryogenics (cooled mirrors) to detect gravitational wave ?

(1)Merits : Reduction of thermal noise and so on (2) How to cool down



### Contents

- 1. Introduction
- 2. Thermal noise
- 3. Other merits
- 4. How to cool down
- 5. Summary



### **1.Introduction**

- List of cryogenic interferometric gravitational wave detectors
- Constructed
  - CLIO (Japan, Sapphire, 100m)
  - KAGRA (Japan, Sapphire, 3km)
- Future plan
  - Voyager (U.S.A., Silicon, 4km, LIGO facility,

Odylio Aguiar in this afternoon ) Einstein Telescope (Europe, Silicon, 10km) Cosmic Explorer (U.S.A., Silicon, 40km) (Michele Punturo in this afternoon)



### **1.Introduction**

- List of cryogenic interferometric gravitational wave detectors
- Constructed
  - CLIO (Japan, Sapphire, 100m)



K.Agatsuma et al., Physical Review Letters 104 (2010) 040602. T. Uchiyama et a;., Physical Review Letters 108 (2012) 141101.



**KAGRA** sapphire

suspension

### **1.Introduction**

List of cryogenic interferometric gravitational wave

e, 100m) hire, 3km, observation starts

on, 4km, LIGO facility) Jurope, Silicon, 10km) .A., Silicon, 40km)



**KAGRA** sapphire

suspension

## **1.Introduction**

List of cryogenic interferometric gravitational wave

There are 4 mirrors. 3 of them are cooled down. The last one will be cooled down within two weeks.

on, 4km, LIGO facility) Jurope, <mark>Silicon</mark>, 10km) .A., <mark>Silicon</mark>, 40km)



# **1.Introduction**

List of cryogenic interferometric gravitational wave



Commissioning with cooled mirror is in progress.

Engineering run of a 3km cavity on 8<sup>th</sup> of June 2019. Duty cycle is 95% at least.

.A., JIICOII, 40KIII)



## **1.Introduction**

List of cryogenic interferometric gravitational wave



Fabian Arellano, Enzo Tapia, Koki Okutomi will present KAGRA vibration isolation system tomorrow afternoon.

on, 4km, LIGO facility) iurope, Silicon, 10km) .A., Silicon, 40km)



# Motivation of cryonic interferometer is reduction of thermal noise.

Story is not so simple ...

Energy equipartition theorem  $\langle x^2 \rangle = k_B T/2$ 

We are interested with power spectrum density in frequency region. Our observation band is between 10Hz and 10kHz. X<sup>2</sup> is integral of power spectrum density in all frequency region.



### Spectrum density of thermal noise of

#### harmonic oscillator

**Q-value** : Magnitude of loss

Higher Q is smaller loss.

Higher Q is<br/>smaller off resonance $10^{-12}$ thermal noise<br/>and better. We interested<br/>with off resonance. $10^{-12}$ 





### Spectrum density of thermal noise

#### of harmonic oscillator

When Q is independent of temperature, power spectrum density in all frequency region is smaller at lower temperature.





# Amplitude of thermal noise (off resonance) is proportional to



In general, **Q-value depends on T** (temperature).

We must investigate how dissipation depends on temperature in cryogenic region.



### **Room temperature second generation interferometer** Fused silica mirror suspended by fused silica fibers

Class. Quantum Grav. 29 (2012) 035003



A V Cumming et al

# **EXAMPRA** 2. Thermal noise

#### **Temperature dependence of Q values**



- R. Nawrodt et al., Journal of Physics: Conference Series 122 (2008) 012008.
- C. Schwarz et al., 2009 Proceedings of ICEC22-ICMC2008.

### Temperature dependence of (T/Q)<sup>1/2</sup>

KAGRA



T. Uchiyama et al., Physics Letters A 261 (1999) 5-11.

- R. Nawrodt et al., Journal of Physics: Conference Series 122 (2008) 012008.
- C. Schwarz et al., 2009 Proceedings of ICEC22-ICMC2008.



#### Important message

### We can not use fused silica for cryogenic interferometer.

New material (Sapphire, Silicon) is necessary for mirror substrate and fibers to suspend mirrors. Challenge !



### Thermal noise of mirror and suspension





### Thermal noise of mirror and suspension





### Thermal noise of mirror Not only substrate but also coating must be taken into account !



Y. Levin, Physical Review D 57 (1998) 659.



Mechanical dissipation generates thermal noise. Loss in substrate and coating Two kinds of loss : Structure, Thermoelastic

Structure : Unknown frequency independent . Measurement of Q-values is only reliable way. P.R. Saulson, Phys. Rev. D 42 (1990) 2437.

Thermoelastic : Coupling of temperature fluctuation and thermal expansion coefficient. We can calculate.

C. Zener, Phys. Rev. 52 (1937) 230; ibid. 53 (1938) 90.



Mechanical dissipation generates thermal noise. Loss in substrate and coating Two kinds of loss : Structure, Thermoelastic

So, there are four kinds of loss (mirror thermal noise). (1)Structure damping in substrate (2)Thermoelastic damping in substrate (3)Structure damping in coating (4)Thermoelastic damping in coating



#### **Structure** damping in **substrate**



- R. Nawrodt *et al.,* Journal of Physics: Conference Series 122 (2008) 012008.
- C. Schwarz et al., 2009 Proceedings of ICEC22-ICMC2008.

# **Thermal noise by structure** damping in **substrate** (Substrate Brownian noise)

KAGRA



Kenji Numata and Kazuhiro Yamamoto,"Chapter 8. Cryogenics", in "Optical Coatings and Thermal Noise in Precision Measurement" Cambridge University Press (2012).

#### Thermal noise by thermoelastic damping

M. Cerdonio et al., Phys. Rev. D 63 (2001) 082003.

KAGRA



Kenji Numata and Kazuhiro Yamamoto,"Chapter 8. Cryogenics", in "Optical Coatings and Thermal Noise in Precision Measurement" Cambridge University Press (2012).

### Thermal noise by thermoelastic damping

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#### Thermal noise by thermoelastic damping

KAGRA



Kenji Numata and Kazuhiro Yamamoto,"Chapter 8. Cryogenics", in "Optical Coatings and Thermal Noise in Precision Measurement" Cambridge University Press (2012).



Structure damping in coating<br/>Y. Levin, Phys. Rev. D 57 (1998) 659.Coating has large contribution to thermal noise<br/>than we expected !This noise is proportional to  $\phi$  1/2.

 $\phi$  is loss strength (it is inverse number of Q-values).

### **EXAGRA 2. Thermal noise** Structure damping in coating (Ta<sub>2</sub>O<sub>5</sub>/SiO<sub>2</sub>)



### Thermal noise by structure damping in coating

KAGRA



KAGRA

#### Thermal noise by thermoelastic damping in coating





### Summary : Sapphire mirror In principle, lower temperature is better.

> 50K
Constant

<20K Enough small





### Summary : Silicon mirror In principle, lower temperature is better.





Mirror substrate and operation temperature

Sapphire, 20 K : CLIO, KAGRA

Silicon, 10 K : Einstein Telescope

Silicon, 120K : Voyager Cosmic Explorer





Mirror substrate and operation temperature

Heat absorption in mirror is an serious issue. How can we avoid that mirror could be hot ?

Typical heat absorption in mirror **1W – 10 W** 

Laser beam





### **120K operation (Silicon)**

Heat absorbed in mirror : Several W

Radiation from mirror is effective. When mirror is surrounded by cold wall (radiation shield), radiation from mirror carries much heat ; 13 W/m<sup>2</sup> at most (Black body radiation). Surface of mirror is 0.3 m<sup>2</sup> at least.




**120K operation (Silicon)** 

Black coating on mirror is necessary. It should have small mechanical dissipation and so on.

Fiber to suspend mirror can be as thin as possible (Fiber must support weight of mirror). Typical diameter is 0.5 mm.





**Below 20K operation (Sapphire, Silicon)** 

Heat absorbed in mirror : about 1 W

Heat extraction : Radiation is useless (*T*<sup>4</sup>). Conduction in fibers Sapphire or silicon has extremely high conductivity (5000 W/m/K).

But, thicker fiber for heat conduction (1.6 mm in diameter, KAGRA) is necessary. When heat transfer is not necessary, 0.5 mm in diameter.



What is an issue of thicker fiber ?

Larger pemdulum thermal noise

Energy of pendulum mode = gravitational potential energy + fiber elastic energy.

Gravitational potential energy has no loss. Elastic energy has loss.

**Thicker fibers** has **larger** elastic energy, loss, and thermal noise.



What is an issue of thicker fiber ?

Larger suspension thermal noise

Energy of pendulum mode = gravitational potential energy + fiber elastic energy.



Gravitational potential energy has no loss. Elastic energy has loss.

Thicker fibers has larger elastic energy, loss, and thermal noise.



What is an issue of thicker fiber ?

Larger pemdulum thermal noise

Energy of pendulum mode = gravitational potential energy + fiber elastic energy.

Gravitational potential energy has no loss. Elastic energy has loss.

**Thicker fibers** has **larger** elastic energy, loss, and thermal noise.



What is an issue of thicker fiber ?

Thermal noise of violin mode

Violin mode : Back action of fiber.

Thicker fiber has large back action. Mode frequency is **lower**.





- Mechanical dissipation in fibers generates suspension thermal noise.
- Two kinds of loss : Structure, Thermoelastic
- Note : Both of them in fiber is different from those in 3 dimensional bulk.



### Pendulum thermal noise (Thermoelastic damping)



KAGRA

### Pendulum thermal noise (Structure damping) Brownian noise



KAGRA



KAGRA



KAGRA



KAGRA





Sapphire, Silicon, 20K Mirror thermal noise is small. Suspension (pendulum and violin mode) thermal noise is an issue (because of thick fiber or heat transmission). Solution (1) Lower frequency interferometer with lower laser power (Einstein Telescope) (2) Small heat absorption mirror Large thermal conductivity fibers





### Sapphire, Silicon, 20K

KAGRA



on).



### No absorption !



### (a) Low heat absorption in mirror

If heat absorption in mirror (not only substrate but also coating) is 10 - 30 times smaller, the fiber can be as thin as possible (More thinner fiber can not support mirror).

Substrate : Small absorption (a few ppm/cm) in small sample was reported. So not impossible ... Coating : It is exactly challenge ...



### (b) Higher thermal conductivity

Size effect : Thermal conductivity is proportional to fiber diameter .

Phonon mean free path is comparable with diameter. It sounds like upper limit of thermal conductivity. But, ..



- (b) Higher thermal conductivity
- It is assumed that phonon is duffed on fiber surface
- as like molecules in vacuum duct.
- But phonon reflection is specular as like light,
- thermal conductivity could be larger.



Thermal conductivity (limited by size effect) of silicon is larger when fiber surface is polished . Phys. Rev. 186, 801 (1969)





#### **Other merits of cooled mirror ?**

(1) Thermal lens(2) Parametric instability



**Thermal lens : Light absorption in mirror Temperature gradient Temperature dependent** of refractive index Wave front distortion **Worse sensitivity Mirror** Laser beam Heat absorption



**Thermal lens : Light absorption in mirror Temperature gradient Temperature dependent** of refractive index Wave front distortion **Worse sensitivity** 





**Thermal lens : Light absorption in mirror Temperature gradient Temperature dependent** of refractive index Wave front distortion Worse sensitivity **Higher or lower** Mirror refractive index Some kind of **Refractive index imperfect** lens ! does not change.

60



**Thermal lens : Light absorption in mirror Temperature gradient Temperature dependent** of refractive index Wave front distortion **Worse sensitivity** Mirror Main laser beam



Thermal lens is a serious problem of room temperature interferometers.

Advanced LIGO and Virgo : System to compensate thermal lens (compensation plate and ring heater) is necessary.

G.M. Harry (for LSC), Classical and Quantum Gravity 27 (2010) 084006.



necessary.

### 3. Other merits

Thermal lens in Sapphire below 20 K T. Tomaru et al., Classical and Quantum Gravity 19 (2002) 2045. Magnitude of thermal lens :  $\beta \mid \kappa$ Temperature coefficient of refractive index ( $\beta$ ) is at least 100 times smaller. Thermal conductivity ( $\kappa$ ) of sapphire at 20 K is 10000 times larger than that of fused silica at 300 K. Magnitude of thermal lens is at least 10<sup>6</sup> times smaller. No system for thermal lens compensation is



**Thermal lens in Silicon** 

- In the case of (below) 20K, thermal lens is neglected.
- In the case of 120K, less effective (careful investigation is necessary).
- Temperature coefficient of refractive index ( $\beta$ ) is comparable with that of fused silica at 300 K.
- Thermal conductivity (κ) of silicon at 120 K is 1000 times larger.
- Magnitude of thermal lens is 10<sup>3</sup> times smaller.



### **Parametric instability**

Radiation pressure



**Optical** mode in cavity

(Large amplitude of other (transverse) optical mode)





**Modulation** 



Parametric instability of cryogenic interferometer is a less serious problem than that of room temperature.

K. Yamamoto et al., Journal of Physics: Conference Series 122 (2008) 012015.

(a) Number of unstable modes is smaller.

(b) More effective passive suppression of instability is possible.



(a) Number of unstable modes is smaller.

Number of unstable modes is proportional to the product of elastic and optical mode densities.

Elastic mode density is inversely proportional to cubic of sound velocity. Sound velocity in sapphire and silicon is about twice times larger than that in fused silica.

Elastic mode density of sapphire and silicon is 4 or 5 times smaller.



(a) Number of unstable modes is smaller.

- Number of unstable modes is proportional to the product of elastic and optical mode densities.
- Optical mode density is smaller when beam radius is smaller.
- Larger beam radius is one of techniques to reduce mirror thermal noise.
- **Cryogenic interferometer** can adopt smaller beam because of small mirror thermal noise.



(b) More effective passive suppression

 of instability is possible.

Passive suppression :

loss on barrel surface of mirror

loss on barrel surface

The increase of thermal noise should be taken into account.

In the case of cooled mirror, more effective suppression is possible.



#### (b) More effective passive suppression



suppression is possible.



(b) More effective passive suppression

 of instability is possible.

Passive suppression :

loss on barrel surface of mirror

loss on barrel surface

The increase of thermal noise should be taken into account.

In the case of cooled mirror, more effective suppression is possible.

# **KAGRA 4. How to cool down**

How to cool down actually ? (KAGRA bias ...)

(1) Cooling bath (or something similar) is necessary. Cooling power is as large as possible. (2) Temperature after cooling down is as low as possible. Heat load (except for mirror absorption) must be negligible. (120K operation; temperature adjustment system is necessary. I skip this topic). (3) Initial cooling time is as short as possible for long observation time.
(1) Cooling bath (or something similar)

Liquid helium, nitrogen ... Large cooling power No vibration (after cool down)

**120K : Only liquid nitrogen is necessary and reuse system is not necessary !** 

So, this could be a solution ....

(1) Cooling bath (or something similar)

Discussion in KAGRA (20K)

Reuse of helium (cycle of liquid and gas of helium): Apparatus with high pressure is necessary. It needs approval by government and license in Japan.

Cost of such apparatus is quite high and complicate.

Liquid helium in tunnel is not so fun ....



(1) Cooling bath (or something similar) for below 20K operation

Cryocooler !

**Heat engine** 

Heat (Q) goes from hot to cold heat bath. Part of heat  $(Q_H-Q_L)$ is converted into work(W).



(1) Cooling bath (or something similar) for below 20K operation

Cryocooler ! Work (W) is applied on cryocooler . Heat (Q) goes from cold to hot heat bath.



Note : Efficiently (cooling power) at lower temperature is smaller because of second law of thermodynamics.



(1)Cooling bath (or something similar)

**Cryocooler : Reverse operation of heat engine** 

(Rigid and heavy) Piston motion generates vibration.

Pulse tube cryocooler : "virtual" piston by valve unit. This "virtual" piston consists of gas ! Small vibration is generated.

Pulse tube cryocooler : 50 W (above 60K) 1W (around 8 K)

C. Tokoku et al., CEC/ICMC2013, 2EPoE1-03, Anchorage, USA (2013).

# KAGRA adopts pulse tube cryocooler. Vibration reduction system was developed by us.

T. Tomaru et al., Classical and Quantum Gravity 21 (2004) S1005.



Figure 3. Vibration-reduction system we have been developing for the PT cryocooler.

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Figure 3. Vibration-reduction system we have been developing for the PT cryocooler.

Mirror

What is cooled down?

We must cool not only mirrors and fibers but also ...

(1) Cryogenic payload : Control of mirror position and alignment for light interference (high sensitivity).

K. Okutomi, Wednesday afternoon



Mirror

What is cooled down?

We must cool not only mirrors and fibers but also ...

(1) Cryogenic payload : Control of mirror position and alignment for light interference (high sensitivity).

K. Okutomi, Wednesday afternoon



What is cooled down?

We must cool not only mirrors and fibers but also

(2) Radiation shield: Cooled wall to avoid attack of 300 K on cryogenic payload.

Radiation shield

Cryogenic payload





(2)Small heat load Actually, extra heat load is always issues ...

Largest one : 300K radiation through hole for laser beam. This hole is comparable with mirror itself; 20cm in diameter. 300K radiation is about 20 W ! It is larger than cryocooler

power around 8K!

Hole for laser beam





Power of 300K radiation is proportional to solid angle of hole. So, 300 K radiation should be small. But actually,....



#### **Cryo duct for KAGRA**

Y. Sakakibara, Ph.D. thesis (2015).



Black coating on inner surface and baffles Only 0.1 W radiation can pass through.



(3)Initial cooling time

It is always serious issue in cryogenic experiment. KAGRA case is introduced.

(c) How to reduce cooling time



- (a) Initial cooling of radiation shield
- In the case of KAGRA
- **Total mass of inner radiation shield is about 700 kg.** C. Tokoku *et al.*, CEC/ICMC2013, 2EPoE1-03, Anchorage, USA (2013).
- Typical specific heat : 1000 J/Kg/K at 300K Dulong-Petit law

- (a) Initial cooling of radiation shield
- Heat extraction power Pulse tube cryocooler : 100 W (above 60K) in KAGRA (two cryocoolers). C. Tokoku *et al.*, CEC/ICMC2013, 2EPoE1-03, Anchorage, USA (2013).
- Calculation shows that it takes about 14 days to cool down (from 300K to 100K).
- Below 100K, cooling time is quite small because of small specific heat (and large thermal conductivity in some case).
- Debye model (Specific heat is proportional

to cubic of temperature.) 93

(a) Initial cooling of radiation shield

Experiment showed that it takes 15 days to cool the radiation shield.

Y. Sakakibara et al., Classical and Quantum Gravity 31(2014)224003.



- (b) Initial cooling of cryogenic payload Payload is isolated thermally.
- In the case of KAGRA, Total mass of payload is 200 kg. Typical specific heat : 1000 J/Kg/K at 300K

**Dulong-Petit law** 

- (b) Initial cooling of cryogenic payload
- Cooling payload above 100 K
- Black body radiation KAGRA : Total surface area of payload is 1 m<sup>2</sup>.
- Radiation power is 460W at most (black coating is necessary) when radiation shields were cooled down.
- It takes only 1 day to cool down cryo payload if radiation shields suddenly cooled !

(b) Initial cooling of cryogenic payload

Cooling payload above 100 K

Thus, temperature of payload is comparable with that of radiation shield while the payload temperature is above 100K.

In the case of Silicon at 120K, this is end of story.

(b) Initial cooling of cryogenic payload

KAGRA : Temperature of payload is comparable with that of radiation shield.

Y. Sakakibara et al., Classical and Quantum Gravity 31(2014)224003.



# (b) Initial cooling of cryogenic payload

Cooling payload below 100 K (in the case of below 20K!)

Radiation does not work (T<sup>4</sup>).

In the case of KAGRA, Heat links (twisted thin AI fibers) between payload and cryocoolers. Thermal conductivity of AI is around 10 K is 10000W/m/K.



- (b) Initial cooling of cryogenic payload
- Cooling payload below 100 K
- Designed heat link can transfer 1W heat power (mirror heat absorption is 1 W).
- Specific heat is smaller at lower temperature. Debye model (Specific heat is proportional to cubic of temperature.)

Typical specific heat : 300 J/Kg/K at 100K KAGRA : Total mass of suspension is 200 kg.





(c) How to reduce cooling time

(i)Short cooling of radiation shield in any cases Payload temperature can follow shield temperature above 100 K owing to radiation.

(ii)Short cooling of payload below 100K It is not necessary in the case of 120K. Y. Sakakibara, Ph.D. thesis (2015).



(c) How to reduce cooling time

(i)Short cooling of radiation shield

Much more cryocoolers ? (KAGRA : 2 cryocoolers for inner shield 2 cryocoolers for payload) Geometrical constrain, vibration

More powerful cryocoolers ? Development, vibration

(c) How to reduce cooling time (ii)Short cooling of payload below 100K

Thicker and shorter heat links Issue is external vibration transmission. KAGRA needs extra vibration isolation system for heat links.



D. Chen et al., Classical and Quantum Gravity 31(2014)224001.

Extra pendulum for vibration isolation

(c) How to reduce cooling time (ii)Short cooling of payload below 100K Thicker and shorter heat links Vibration isolation system for KAGRA heat links.

T. Yamada et al., https://gwdoc.icrr.u-tokyo.ac.jp/cgibin/private/DocDB/ShowDocument?docid=9002

Sapphire

mirror

Vibration

isolation

system

for heat

**Pure aluminum** 

links

heat links

(c) How to reduce cooling time (ii)Short cooling of payload below 100K If you develop better heat link vibration isolation system that that of KAGRA, you can adopt thicker and shorter heat links and initial cooling times is shorter.

Sapphire mirror

Pure aluminum heat links

isolation

system

for heat

links

(c) How to reduce cooling time
(ii)Short cooling of payload below 100K
Heat path with thermal switch

Initial cooling : Thermal switch is turned on. Heat path works.

After cooling down : Thermal switch is turned off. Heat path is cut.

Thermal switch is quite tricky part ....

 (c) How to reduce cooling time
(2)Short cooling of payload below 100K Heat path with thermal switch

Gas : Radiation shield should keep gas. All holes for laser beam and bar from room temperature part are closed. During cooling, main laser beam can not observe drift of mirror. Super insulator absorbs helium gas. It takes longer time to evacuate helium gas.
# **KAGRA 4. How to cool down**

 (c) How to reduce cooling time
 (2)Short cooling of payload below 100K Heat path with thermal switch

**Mechanical** thermal switch between payload and crycoolers Large heat contact during initial cooling (force) Large thermal isolation after initial cooling (soft metal for contact disturbs detachment) Thermal switch on suspended object **Direction and position of mirror should be** changed after this switch is turned off. Mechanism must work at cryogenic temperature. 109





### Merits of cryogenic interferometer (Comparison with 300K interferometer)

(1) Small mirror (coating) thermal noise(2) Small thermal lens(3) Less serious parametric instability

### Challenges

(1) New martials (sapphire, silicon) as substrate
(2) Small vibration cooling bath or cryocoolers
(3) Cryoduct to terminate 300K radiation
(4) Shorter cooling time of radiation shield





**Operation temperature** 

Below 20K operation
We can enjoy merits fully.
What we must investigate or overcome
(1) Thicker fiber for heat transmission
(2) Heat link vibration isolation
(3) Cooling time below 100K

#### **120K operartion**

Since radiation cooling is **effective**, issues below 20K does not matter. But some merits are missed ... (Coating mechanical loss reduction is necessary).



### The book about coating thermal noise was published on 2012 !

**Cambridge University Press** 

Chapter 8 (K. Numata and K. Yamamoto) "Cryognics"

#### Optical Coatings and Thermal Noise in Precision Measurement

EDITED BY Gregory Harry Timothy P. Bodiya Riccardo DeSalvo

CAMBRIDGE



# Thank you for your attention !



## **1.Introduction**

	aLIGO / AdV	A+/V+	KAGRA	CE 1	CE 2	ET-LF	ET-HF
Arm Length [km]	4/3	4	3	40	40	10	10
Mirror Mass [kg]	40 / 42	40	23	320	320	211	200
Mirror Material	silica	silica	sapphire	silica	silicon	silicon	silica
Mirror Temp [K]	295	295	20	295	123	10	290
Suspension Fiber	0.6m/0.7m	0.6m	0.35m	1.2m	1.2m	2m	0.6m
	SiO2	SiO2	Al2O3	SiO2	Si	Si	SiO2
Fiber Type	Fiber	Fiber	Fiber	Fiber	Ribbon	Fiber	Fiber
Input Power [W]	125	125	70	150	220	3	500
Arm Power [kW]	710 / 700	750	350	1400	2000	18	3000
Wavelength [nm]	1064	1064	1064	1064	1550	1550	1064
NN Suppression	1	1	1	10	10	1	1
Beam Size [cm]	(5.5/6.2)/6	5.5/6.2	3.5/3.5	12/12	14/14	9/9	12/12
SQZ Factor [dB]	0	6	foreseen	10	10	10	10
F. C. Length [m]	none	300	unknown	4000	4000	10000	500

T. Uchiyama et al., Physics Letters A 261(1999)5.



# 2. Thermal noise

#### In the case of KAGRA (Sapphire, 20K) ....

